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Thickness-dependent phase transition in thin nematic films

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Using light scattering, the thickness dependence of the isotropic-nematic phase transition temperature \( T_{NI} \) in a thin film of octylcyanobiphenyl (8CB) is studied in two distinct geometries: with and without strain. We observed a large stress induced shift in \( T_{NI} \), as a function of the film thickness \( d \). At \( d \approx 0.3 \mu m \) a crossover in the behavior of \( T_{NI} \) as a function of thickness is observed, which can be attributed to a competition between strain and anchoring forces. [S1063-651X(96)08311-0]

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The effects of confinement on the phase transitions in liquid crystals have attracted much attention recently [1–4]. In particular, calorimetric and light scattering experiments on liquid crystals in porous media indicate a shift \( \Delta T_{NI} \) of the isotropic-nematic transition and a possible change from a first order to a continuous transition. This last observation appears to depend on the type of porous matrix. For example, Iannacchione et al. find a second order transition in porous glass [4], whereas in Anopore the transition is of first order [1]. To understand these observations, both the confinement and the randomness of the porous medium are important. Confinement effects will in general lead to a \( 1/R^2 \) depression of the transition temperature, whereas a random field leads to a suppression of the first order character. Both aspects have been observed [1–4].

In this paper we present a study of the confinement effects of the isotropic-nematic phase transition using a well defined planar geometry. This enables us to control the thickness and the surface induced ordering independently. The influence of ordering or disordering on the surfaces on the isotropic-nematic phase transition temperature in 5CB in a cell with two identical boundaries has been studied by Yokoyama [5]. His measurements were consistent with the calculations of Sheng [6] and Poniewierski et al. [7], and showed a \( 1/d \) and \( -1/d^2 \) dependence of the \( \Delta T_{NI} \) for an ordering and disordering surface, respectively.

We have examined the case of two different surface orientations, and have observed a \( \Delta T_{NI} \) following a combination of \( -1/d^2 \) and \( 1/d \) dependence for thicknesses larger than 0.3 \( \mu m \), and showing a \( -1/d \) dependence for smaller thicknesses. Here \( d \) is the separation between the two surfaces. In contrast, when both surfaces induce the same orientation, no shift of \( T_{NI} \) is observed. The results are in qualitative agreement with a Landau model introduced by Sluckin et al. [8], where two competing orientations introduce a stress term that is responsible for the observed \( -1/d^2 \) dependence. Sluckin et al. also predicted a crossover to a \( 1/d \) thickness dependence for small \( d \). The absence of a measurable shift in the cell with two identical boundaries is consistent with the measurements by Yokoyama [5].

For the experiments we used octylcyanobiphenyl (8CB), which has a bulk nematic-isotropic phase transition at 41°C. To prepare a homeotropic and planar alignment, the 8CB was spread on a nylon coated glass substrate. The nylon coated surface induces a planar ordering, whereas the free surface gives a homeotropic alignment. The 8CB was deposited using iso-propanol as a solvent and formed flat, pancake-like droplets. For the larger thicknesses, the film thickness was determined by counting Newton’s rings; for the very thin films, the thickness was calculated from the known amount of bulk material and the measured size of the 8CB droplet. The accuracy of this determination was checked by also using it for thicker films. For the planar-planar geometry, we used a flat fused quartz substrate on the one side, and a long focal length (\( f=2 m \)) glass lens as the other surface. In this way the cell contained a continuous variation of thicknesses from \(<0.02 \mu m \) in the center, to \( \sim 10 \mu m \) (at 7 mm from the center). Here the thickness increases as \( r^2 \), where \( r \) is the distance with respect to the center. The cell was filled at 50°C using capillary action in the isotropic phase.

We used static light scattering to determine the temperature of the isotropic-nematic phase transition. The liquid crystal is placed between crossed polarizers, and the scattered intensity is measured under an angle of \( \sim7° \) with respect to the transmitted beam. In this geometry there is almost no scattering in the isotropic phase. In the nematic phase, however, a finite amount of scattering due to order parameter fluctuations is measured. Figure 1 shows the measured scattering intensity as a function of the temperature for several cell thicknesses. At the phase transition we observe a sudden jump in the scattering intensity, which for thicker layers is accompanied by intensity fluctuations.

Even for the smallest thicknesses, the transition appears to be first order judging from the small but discontinuous step in the scattering intensity at \( T_{NI} \). A gradual transition to a more second-order-like transition cannot, however, be excluded within the present accuracy.

Figure 2 shows the shift of the isotropic-nematic phase transition temperature as a function of the film thickness, in the case of two different boundaries. We observe two regimes. For larger thicknesses (\( >0.3 \mu m \)) the shift is a combination of a \( 1/d \) (surface ordering effect) and a \( -1/d^2 \) de-
FIG. 1. Light scattering intensity vs temperature for different film thicknesses: $d=0.5 \, \mu m$ (○), $d=0.25 \, \mu m$ (+), and $d=0.02 \, \mu m$ (□). $T_{NI}$ is the isotropic-nematic phase transition temperature. The lines are guides to the eye.

The isotropic-nematic phase transition temperature, relative to its bulk value $41.2^\circ C$, vs thickness in strained 8CB films. The transition temperature shifts to lower values for $d \leq 0.5 \, \mu m$. A schematic view of the film configuration is shown in the inset: flat 8CB pancake-like droplets on the substrate.

FIG. 2. The isotropic-nematic phase transition temperature, relative to its bulk value $41.2^\circ C$, vs thickness in strained 8CB films. The transition temperature shifts to lower values for $d \leq 0.5 \, \mu m$. A schematic view of the film configuration is shown in the inset: flat 8CB pancake-like droplets on the substrate.

FIG. 4. The isotropic-nematic phase transition temperature, relative to its bulk value $40.8^\circ C$, vs thickness for a strainless 8CB layer. The inset schematically shows the cell configuration: 8CB between a lens and a flat substrate.

dependence (caused by strain). This can clearly be seen in Fig. 3, where $\Delta Td$ is plotted versus $1/d$. Fitting the data yields

$$\Delta Td = A - \frac{B}{d},$$

with $A=0.17 \pm 0.10 \, \mu m \, K$, $B=0.14 \pm 0.05 \, \mu m^2 \, K$, and $d$ in $\mu m$. For thicknesses smaller than $0.3 \, \mu m$, however, the dependence has changed into a $-1/d$ behavior,

$$\Delta T \sim - \frac{C}{d},$$

with $C=0.29 \pm 0.03 \, \mu m \, K$ and $d$ in $\mu m$. In the situation where we have identical boundaries, we observed no shift in the phase transition temperature within the accuracy of our measurements ($\pm 0.1^\circ C$) (Fig. 4). These two observations lead to the conclusion that the temperature shift, observed in the first situation, must be due to stress induced by the forced variation of the orientation within the sample.

Following Sluckin et al. [8] one expects two thickness regimes for capillary condensation in a restricted planar geometry with different orientations induced by the walls. A crossover between these two regimes occurs at a certain thickness $d_c$.

For thicknesses larger than $d_c$ two terms are important: (1) a capillary condensation term, which comes from the Kelvin equation and contains the surface tensions $\gamma_N$ and $\gamma_I$, where the subscripts denote the nematic and isotropic phase, respectively; (2) a stress term, which causes a varying director orientation within the nematic layer and is a linear function of the Frank elastic constant $K$. The phase transition takes place at a temperature $T_{NI} + \Delta T$, where

$$\Delta T = \frac{T_{NI}}{L} \left[ (\gamma_I^2 - \gamma^2) + (\gamma_I^2 - \gamma^2) \frac{\pi^2 K}{4d^2} \right].$$

For thicknesses smaller than $d_c$, the phase transition takes place at a temperature $T_{NI}$, where

$$\Delta T = \frac{T_{NI}}{L} \left[ (\gamma_I^2 - \gamma^2) \right].$$
where $L$ is the latent heat at the isotropic-nematic transition, and the indices 1 and 2 indicate the two separate boundaries.

At $d=d_c$, however, the cost of varying the director is higher than that of changing the boundary condition at the boundary with the smallest anchoring constant $W$. This means that for $W_1 < W_2$, $(\gamma_2)_{1} \cdot W_1$ should be replaced by $(\gamma_2)_{1} + W_1$. In the regime where $d=d_c=(K/W_1)$, we therefore expect

$$\Delta T = \frac{T_{NI}}{L}\left(\frac{(\gamma_1-\gamma_N)_{1} + (\gamma_1-\gamma_N)_{2} - W_1}{d}\right).$$

(4)

Note that $d_c$ equals the extrapolation distance $L_1$. The crossover between the two behaviors can be gradual or in the form of a phase transition [8].

For the calculation of $\Delta T$ we use the Young-Laplace equation for the surface tension at wall $\mathit{i}$ [7]:

$$\gamma_N^i \sin \theta_N^i = (\gamma_1-\gamma_N)_{i} - (\gamma_1-\gamma_N)_{N} \cos \theta_N^i,$$

(5)

with $\gamma_N^i$ the surface tension of the $Ni$-interfacial layer and $\theta_N^i$ the angle of the $Ni$ interface with respect to wall $\mathit{i}$.

Comparison between these calculations and our measurements shows a good qualitative agreement. Furthermore, the ratios between the three terms caused by capillary condensation, strain and anchoring, respectively, are consistent with the expectations, when we use $\gamma_N=9.5\times10^{-6}$ J/m$^2$ [9], $K=3\times10^{-12}$ N [10], $W=2.5\times10^{-5}$ J/m$^2$ [values measured by others are $W=(1.0\pm0.5)\times10^{-5}$ J/m$^2$ [11] and $W>6\times10^{-5}$ J/m$^2$ [9]], and $\cos \theta_N^i + \cos \theta_W^i = 1$ (i.e., slightly ordering surfaces). From these values of $K$ and $W$ we can calculate $d_c$ to be $0.12 \mu m$, which is in reasonable agreement with the experimentally found value of $0.3 \mu m$. However, our measured temperature shifts are almost two orders of magnitude larger than calculated, using $T_{NI}=314$ K and $L=1.36\times10^6$ J/m$^3$ (value for 5CB [5]).

These observations seem to lead to the conclusion that for a film with one free surface there is an effective latent heat which is much smaller than the bulk value, given above. In systems containing two cell walls [5] temperature shifts have never been observed for thicknesses as large as $0.4 \mu m$ and the latent heat equals the bulk latent heat. This is also confirmed by our measurements on 8CB layers in a cell, where the bulk latent heat should be used to account for the absence of a measurable temperature shift.

At this moment it is not clear why a free surface would lead to such a small latent heat. We can only refer to experiments done in porous media where the measured latent heat is found to be slightly smaller than the bulk value [12].

In conclusion, we have observed the competition between capillary condensation, strain and anchoring. The measured behavior of the shift in the $IN$-phase transition temperature as a function of thickness is qualitatively consistent with the theoretical predictions of Sluckin et al. [8]. Also the ratios between the different terms: capillary condensation, strain and anchoring and the observed critical thickness agree with the expectations. However, the free surface of the 8CB films seems to lead to a temperature shift that is much larger than the temperature shifts measured in stainless cells.

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