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Scattering by flexural phonons in suspended graphene under back gate induced strain

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Abstract
We have studied electron scattering by out-of-plane (flexural) phonon modes in doped suspended graphene and its effect on charge transport. In the free-standing case (absence of strain) the flexural branch shows a quadratic dispersion relation, which becomes linear at long wavelength when the sample is under tension due to the rotation symmetry breaking. In the non-strained case, scattering by flexural phonons is the main limitation to electron mobility. This picture changes drastically when strains above \( \bar{u} = 10^{-4} \text{nm}(10^{12} \text{cm}^{-2}) \) are considered. Here we study in particular the case of back gate induced strain, and apply our theoretical findings to recent experiments in suspended graphene.

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1. Introduction
Graphene is a novel two dimensional material whose low-temperature conductivity is comparable to that of conventional metals [1], despite much lower carrier concentrations. Interactions with the underlying substrate seem to be the main limitation to electron mobility, and recent experiments on suspended samples show a clear enhancement of mobility (more than one order of magnitude) at low temperatures [2,3].

In suspended graphene carbon atoms can oscillate in the out-of-plane direction leading to a new class of low-energy phonons, the flexural branch [3,6]. In the free standing case, these modes show a quadratic dispersion relation, so there is a high number of these low-energy phonons and the graphene sheet can be easily deformed in the out-of-plane direction. For this reason it can be expected that flexural phonons are the intrinsic strongly T-dependent scattering mechanism which ultimately limits its mobility at room temperature [2]. However, since the scattering process always involves two flexural phonons, a membrane characteristic feature, its effect could be reduced, specially at low temperatures [4,5].

In the present manuscript we analyse theoretically the contribution of flexural modes to the resistivity in suspended graphene samples. Our results suggest, indeed, that flexural phonons are the main source of resistivity in this kind of samples. We also show how this intrinsic limitation is reduced by the effect of strain. A quantitative treatment of back gate induced strain where graphene is considered as an elastic membrane with clamped edges is given.

2. The model
In order to describe long-wavelength acoustic phonons graphene can be seen as a two dimensional membrane whose elastic properties are described by the free energy [2,3]

\[
F = \frac{1}{2} \kappa \int dxdy(\nabla^2 h)^2 + \frac{1}{2} \int dxdy(\lambda u_{\alpha\alpha}^2 + 2\mu u_{ij}^2). \tag{1}
\]

where \( \kappa \) is the bending rigidity, \( \lambda \) and \( \mu \) are Lamé coefficients, \( h \) is the displacement in the out of plane direction, and \( u_{ij} = 1/2(\partial_i u_j + \partial_j u_i + (\partial_i h)(\partial_j h)) \) is the strain tensor. Typical parameters for graphene [2] are \( \kappa \approx 1 \text{eV}, \) and \( \mu \approx 3\lambda \approx 9 \text{eV} \text{Å}^{-2}. \) The mass density is \( \rho = 7.6 \times 10^{-7} \text{Kg/m}^2. \) The longitudinal and transverse in-plane phonons show the usual linear dispersion relation with sound velocities \( v_L = \sqrt{\frac{\lambda + 2\mu}{\rho}} \approx 2.1 \times 10^4 \text{m/s} \) and \( v_T = \sqrt{\frac{\mu}{\rho}} \approx 1.4 \times 10^4 \text{m/s}. \) Flexural phonons have the dispersion

\[
\omega^F_q = \alpha |q|^2 \tag{2}
\]

with \( \alpha = \sqrt{\frac{\kappa}{\rho}} \approx 4.6 \times 10^{-7} \text{m}^2/\text{s}. \) The quadratic dispersion relation is strictly valid in the absence of strain. At finite strain the dispersion relation of flexural phonons becomes linear at long-wavelength due to rotation symmetry breaking. Let us assume a slowly varying strain field \( u_{ij}(r) \). The dispersion in Eq. (2) is changed to:

\[
\omega^F_q(r) = |q|\sqrt{\frac{\kappa}{\rho}}|q|^2 + \frac{\lambda}{\rho} u_{ij}(r) + \frac{2\mu}{\rho} u_{ij}(r) \frac{q_i q_j}{|q|^2}. \tag{3}
\]

In order to keep an analytical treatment we assume uniaxial strain \( \epsilon_{xx} \equiv u \), and the rest of strain components
zero), and drop the anisotropy in Eq. (3) by considering the effective dispersion relation

\[ \omega_q^F = q \sqrt{\alpha^2 q^2 + \bar{v}_L^2}. \]  

(4)

Long-wavelength phonons couple to electrons in the effective Dirac-like Hamiltonian \([10]\) through a scalar potential (diagonal in sublattice indices) called the deformation potential, which is associated to the lattice volume change and hence it can be written in terms of the trace of the strain tensor \([11, 12]\)

\[ V(r) = g_0 \left[ u_{xx}(r) + u_{yy}(r) \right] \]  

(5)

where \(g_0 \approx 20 - 30 \text{ eV} \) \([11]\). Phonons couple also to electrons through a vector potential associated to changes in bond length between carbon atoms, and whose components are related with the strain tensor as \([12, 14]\)

where \(\alpha \approx 1.4 \text{ Å}\) is the distance between nearest carbon atoms, \(\beta = -\partial \log(t)/\partial \log(a) \approx 2 - 3 \) \([13]\), and \(t \approx 3 \text{ eV}\) is the hopping between electrons in nearest carbon \(\pi\) orbitals.

Quantizing the displacements fields in terms of the usual bosonic \(\hat{a}_q^{\dagger}\) operators for phonons of momentum \(q\) we arrive at the interaction Hamiltonian. The term which couples electrons and flexural phonons reads

\[ H_{e-ph} = \sum_{k.k',q,q'} \left[ \sum_{a,b} \left( a_F^{q'\dagger} a_{F}^{q} \right) \left( a_F^{q'} a_{F}^{q} \right) \delta_{k,k'-q-q'} \right] \times \left[ \sum_{c} V_{1,F,q'}^F c_k^{c \dagger} c_k + \left( V_{2,F,q}^F a_{k}^\dagger b_{k} + h.c. \right) \right], \]  

(7)

where operators \(a_k^\dagger\) and \(b_k^\dagger\) create electrons in Bloch waves with momentum \(K\) in the \(A\) and \(B\) sublattices respectively. The matrix elements are

\[ V_{1,F,q}^F = -g_0 \frac{\cos(\phi - \phi')}{2\epsilon(q + q')} \left( \frac{\hbar}{2V_F \sqrt{\omega_q \omega_{q'}}} \right), \]  

\[ V_{2,F,q}^F = -v_F \frac{\hbar \delta q}{a} \left( \frac{\hbar}{2V_F \sqrt{\omega_q \omega_{q'}}} \right), \]  

(8)

where \(\phi = \arctan(q_y/q_x)\) and \(V\) is the volume of the system. The effect of screening has been taken into account in the matrix elements of deformation potential through a Thomas-Fermi-like dielectric function \(\varepsilon(q) = 1 + \varepsilon^2 D(E_F) q^2\), where \(D(E_F)\) is the density of states at Fermi energy. Note that \(g = g_0/\varepsilon(k_F) \approx 3 \text{ eV}\) in agreement with recent \(ab\) \(initio\) results \([13]\).

3. Resistivity in the absence of strain

From the linearized Boltzmann equation we can calculate the resistivity as \(g = \frac{\hbar^2}{e^2},\) where \(\hbar^2\approx 10^6 \text{ m/s}\) is the Fermi velocity. Our aim is to compute the inverse of the scattering time of quasiparticles, given by \(\tau^{-1} = \sum_{k} (1 - \cos \theta_{k,k'}) \omega_{k} \), where \(\omega_{k} \) is the scattering probability per unit time, which can be calculated through the Fermi’s golden rule. For scattering processes mediated by two flexural phonons, within the quasi-elastic approximation, we obtain

\[ \tau_{k,k'}^{-1} = \frac{4\pi}{3} \sum_{q} \sum_{q'} |V_{1,F,q}^F|^2 \delta_{q,q'} \times n_q (n_q + 1) \delta_{q',q-q'} \delta (E_k - E_{k'}) \]  

(9)

where \(f_{1,F}^{(1)} = 1 + \cos \theta_{k,k'}\) and \(f_{2,F}^{(2)} = 1\), \(n_q\) is the Bose distribution, and \(E_k = v_F k\) is the quasi-particle dispersion for the Dirac-like Hamiltonian \([10]\). Eq. (9) is valid in the high \(T\) limit to be specified in the following.

In order to obtain analytical expressions for the scattering rates it is useful to introduce the Bloch-Grüneisen temperature \(T_{BG}\). If we take into account that the relevant phonons which contribute to the resistivity are those of momenta \(q \geq 2k_F\) then we have \(k_F T_{BG} = \hbar \omega_{2k_F}\) for in-plane longitudinal (transverse) phonons \(T_{BG} = 57\sqrt{\pi} K\) \((T_{BG} = 38\sqrt{\pi} K)\), where \(n\) is expressed in \(10^{12} \text{ cm}^{-2}\). For flexural phonons in the absence of strain \(T_{BG} = 0.1n K\). From the last expression it is obvious that for carrier densities of interest the experimentally relevant regime is \(T \gg T_{BG}\), so let us concentrate on this limit.

In the case of scattering by in-plane phonons at \(T \gg T_{BG}\) the scattering rate is given by \([16]\)

\[ \frac{1}{\tau_I} \approx \left[ \frac{g^2}{2 v_L^2} + \frac{\hbar^2 v_F^2 \beta^2}{4a^2} \left( \frac{1}{v_L^2} + \frac{1}{v_F^2} \right) \right] \frac{E_F}{2\hbar v_F^2} k_B T, \]  

(10)

where now \(g \approx 3 \text{ eV}\) is the screened deformation potential constant. At \(T < T_{BG}\) the scattering rate behaves as \(\tau^{-1} \sim T^4\), while only the gauge potential contribution is taken into account since the deformation potential is negligible in this regime due to screening effects \((\tau^{-1} \sim T^6)\).

In the case of flexural phonons in the non-strained case \((\text{in practice} \, \bar{u} \ll 10^{-4} \text{ with} \, n \in 10^{12} \text{ cm}^{-2})\), the scattering rate at \(T \gg T_{BG}\) reads \([10]\)

\[ \frac{1}{\tau_F} \approx \left[ \frac{g^2}{2} + \frac{\hbar^2 v_F^2 \beta^2}{4a^2} \right] \frac{k_B T^2}{64\pi \hbar^2 \kappa E_F} \ln \left( \frac{k_B T}{\hbar \omega_c} \right) \]  

\[ + \left[ \frac{g^2}{4} + \frac{\hbar^2 v_F^2 \beta^2}{4a^2} \right] \frac{k_B T E_F}{32\pi v_F^2 \kappa^2 \hbar^2} \ln \left( \frac{k_B T}{\hbar \omega_c} \right), \]  

(11)

where we have taken into account two contributions, one coming from the absorption or emission of two thermal phonons, and other involving one non-thermal phonon. The first one dominates over the second at \(T \gg T_{BG}\). It is necessary to introduce an infrared cutoff frequency \(\omega_c\), where for small but finite strain \(\bar{u} \ll 10^{-4} \text{ and} \, \omega_c \approx 10^{12} \text{ cm}^{-2}\) is just the frequency below which the flexural phonon dispersion becomes linear.

From Eq. (10) we deduce a resistivity which behaves as \(g \sim T\), with no dependence on \(n\), whereas from Eq. (11)
we have (neglecting the logarithmic correction) $\varrho \sim T^2/n$, as it was deduced for classical ripples in [7]. As it can be seen in Fig. 3 the resistivity due to scattering by flexural phonons dominates over the in-plane contribution. However, this picture changes considerably if one considers strain above $10^{-4}n(10^{12}\text{cm}^{-2})$, as is discussed in the next section.

4. Resistivity at finite strains

4.1. Scattering rate

The Bloch-Grüneisen temperature for flexural phonons at finite strains $\tilde{u} \gtrsim 10^{-4}n(10^{12}\text{cm}^{-2})$ is $T_{BG} = 28\sqrt{\text{um}}$ K. In the relevant high-temperature regime, $T \gg T_{BG}$ the scattering rate can be written as [10]

$$\frac{1}{\tau_{F\text{str}}} \approx \left(\frac{g^2}{4} + \frac{\hbar^2 c_F^2 \beta^2}{4a^2}\right) \frac{E_F(k_B T)^4}{16\pi^2\hbar^4c_F^6v_F^6n^3} \times \left[R_2\left(\frac{\alpha k_B T}{\hbar v_F}\right) + R_4\left(\frac{\alpha k_B T}{\hbar v_F}\right)\right]$$

(12)

where $R_n(\gamma) = \int_0^\infty dx x^n e^{-x^2 - \gamma^2}$. The two terms in Eq. (12) come from the same processes as in Eq. (11) described above. It is possible to obtain asymptotic analytical expressions for Eq. (12). For instance, in the limit $T \ll T^* = \frac{\hbar v_F}{\alpha k_B \tilde{u}} \approx 7 \times 10^3\tilde{u}$ K the scattering rate behaves as $\tau^{-1} \sim \frac{T^2}{\tilde{u}^2}$, whereas in the opposite limit it behaves as $\tau^{-1} \sim \frac{T^2}{\tilde{u}^2}$. The temperature $T^*$ characterises the energy scale at which the flexural phonon dispersion under strain Eq. (11) cross over from linear to quadratic.

It is pertinent to compute the crossover temperature $T^{**}$ above which scattering by flexural phonons dominates when strain is induced. This can be inferred by comparing Eq. (11) with Eq. (12) and imposing $\tau_{F\text{str}}/\tau_{F\text{str}} \approx 1$. The numerical solution give for the corresponding crossover $T^{**} \approx 10^6\tilde{u}$ K. Since $T^{**} \gg T^*$ we can use the respective asymptotic expression for Eq. (12), $\tau^{-1} \sim \frac{T^2}{\tilde{u}^2}$ to obtain $T^{**} \approx 32\pi k_B/k_B \approx 10^6\tilde{u}$ K. A remarkable conclusion may then be drawn: scattering due to flexural phonons can be completely suppressed by applying strain as low as $\tilde{u} \gtrsim 0.1\%$.

4.2. Back gate induced strain

In order to compute the strain induced by the back gate we consider the simplest case of a suspended membrane with clamped edges. A side view of the system is given in the inset of Fig. 4.3.

The static height profile is obtained by minimising the free energy, Eq. (1) in the presence of the load $P = e^2n^2/(2\varepsilon_0)$ due to the back gate induced electric field. The built up strain is related with the applied load as [8, 15],

$$\tilde{u} = \frac{PL^2}{8h_0(\lambda + 2\mu)} \approx 5 \times 10^{-5}\frac{[n(10^{12}\text{cm}^{-2})L(\mu\text{m})]^2}{h_0(\mu\text{m})},$$

(13)

where $L$ is the length of the trench over which graphene is clamped and $h_0$ is the maximum deflection (see the inset of Fig. 4.4). We assume the length of the suspended graphene region in the undeformed case to be $L + \Delta L$, where the $\Delta L$ can be either positive or negative. Under the approximation of nearly parabolic deformation (which can be shown to be the relevant case here [18]) the maximum deflection $h_0$ is given by the positive root of the cubic equation

$$h_0^3 - \frac{3}{8}L\Delta L h_0 = \frac{3PL^4}{64(\lambda + 2\mu)},$$

(14)

with trench/suspended-region length mismatch $\Delta L$ such that $\Delta L \ll L$. If $\Delta L = 0$ then Eq. (13) can be easily solved and we obtain for strain

$$\tilde{u} = \frac{1}{2\sqrt[3]{L}} \frac{PL}{\lambda + 2\mu} \approx 2 \times 10^{-3}(n^2L)^{2/3},$$

(15)

with $n$ in $10^{12}\text{cm}^{-2}$ and $L$ in $\mu\text{m}$.
tem if samples can also fall in the category of non-strained systems. We argue that the experimental data in Ref. [4] can be understood within experimental reach. In the next section we will show that the experimental results in Ref. [4] can be understood within this framework. However, note that the original samples can also fall in the category of non-strained systems if $\Delta L > 0$. This is clearly seen in Fig. 4.2 for $\Delta L$ as small as $\Delta L/L \approx 0.3\%$.

4.3. Resistivity estimates: comparison with experiment

Bolotin et al. [4] have recently measured the temperature-dependent resistivity in doped suspended graphene. The experimental results are shown in the left panel of Fig. 4.3 in linear scale, and the inset shows the same in log-log scale. In Ref. [4] the resistivity was interpreted as linearly dependent on temperature $\varrho \sim T$ to $\varrho \sim T^2/\bar{u}$ due to flexural phonons at $T^{**} \approx 100$ K, well within experimental reach. In the next section we will argue that the experimental data in Ref. [4] can be understood within this framework. However, note that the original samples can also fall in the category of non-strained systems if $\Delta L > 0$. This is clearly seen in Fig. 4.2 for $\Delta L$ as small as $\Delta L/L \approx 0.3\%$.

5. Conclusions

Our theoretical results suggest that scattering by flexural phonons constitute the main limitation to electron mobility in doped suspended graphene. This picture changes drastically when the sample is strained. In that case, strains with not too large values, as those induced by the back gate, can suppress significantly this source of scattering. This result opens the door to the possibility of possibly modifying locally the resistivity of a suspended graphene by strain modulation.

References

[16] Derivation details will be given elsewhere.
[19] We used $\varrho = 3\bar{u}$, $\beta = 3$, $\Delta L = 0$, and $L = 0.3\mu$m. The latter parameter is interpreted as an effective length mimicking the difference between our two side clamped membrane and the real four point clamped device.

Figure 3: Left: Temperature dependent resistivity from Ref. [4] at different gate voltages; the inset shows the same in log-log scale. Right: Result of Eq. (16); the inset shows the back gate induced strain as given by Eq. (15).